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DAVID W. TAYLOR NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER

Bethesda, Md. 20084

ELASTOMERS FOR SERVICE AS SEALS FOR ENGINE LUBRICANTS AND HYDRAULIC FLUIDS

by William Klemens and Paul Lagally

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> MATERIALS DEPARTMENT Annapolis RESEARCH AND DEVELOPMENT REPORT

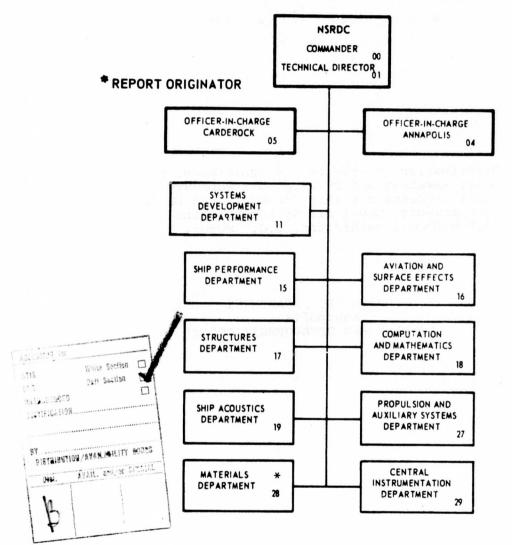
February 1976

Report MAT-75-78

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Six poly(fluoroalkoxy) phosphazene (PNF) elastomers were examined against a Viton control as candidates for O-rings which can function between -65°F and +350°F. All PNF-compounds were based on a single polymer manufactured by Firestone Tire and Rubber Company. Two compounds were purchased from Firestone and three from Horizons, Inc.; Nichols Engineering, Inc. supplied a proprietary compound. These six wulcanizates represent the most (over)

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20. ABSTRACT (Cont) (P14734)

advanced compound technology for PNF. Tensile data clearly show that these six PNF compounds cannot withstand hydraulic fluid MIL-H-83282A at +350° F. The tensile strengths deteriorate rapidly with immersion time. By contrast, the Viton control shows almost no change. The compression set characteristics of the six PNF compounds show a significant improvement over those previously examined in previous work. Nevertheless, it is expected that compression set, too, would suffer with increased conditioning time at +350° F in the hydraulic fluid. The low temperature flexibility of PNF vulcanizates is excellent, but other important physical properties show of vious deficiencies, particularly after conditioning in hydraulic fluid at +350° F.

(Authors)

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ADMINISTRATIVE INFORMATION

This work was accomplished under NAVAIR WF 54 544 205, Work Unit 2841-516, as outlined in reference (a). The technical coordinator is Mr. J. Gurtowski, NAVAIR (AIR 52032C); the project engineers are Dr. Paul Lagally and Messrs. W. Klemens and H. S. Preiser.

ADMINISTRATIVE REFERENCE

(a) NAVAIR Program Summary of 1 May 1974

LIST OF ABBREVIATIONS

- fluorocarbon rubber FKM hr/° F - hour per degrees Fahrenheit in-lbs/in³ - inch-pound per cubic inch min/° F - minute per degrees Fahrenheit - milliliter ml - millimeter mm - nitrile-butadiene rubber NBR PNF - poly(fluoroalkoxy)phosphazene psi - pounds per square inch

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BACKGROUND

Nitrile-butadiene rubber (NBR) O-rings have had an acceptable service life in aircraft hydraulic systems which function between -65° F (-53.9° C) and +225° F (+107.2° C). However, service life is reduced and maintenance requirements are increased at temperatures which approach and exceed +300° F (+148.9° C) in the more advanced aircraft. Viton fluorocarbon rubber (FKM) O-rings function up to +450° F (+232° C) but lose their flexibility below -20° F (-28.9° C). Development is presently directed toward materials which can function as O-rings between -50° F (-45.6° C) and +350° F (+176.6° C).

Over the last several years, attention has focused on inorganic polyphosphazene elastomers which are stable over a wide temperature range. The Firestone Tire and Rubber Company manufactures pilot quantities of the organic substituted poly (fluoroalkoxy) phosphazene, trade name PNF. Earlier work revealed that the physical properties of three compounds made from this polymer (two from Horizons, Inc., and one from Firestone) degraded severely when immersed at +350° F (+176.6° C) in the hydraulic fluid specified in MIL-H-83282 Amendment 2 (for service between -40° F (-40.0° C) and +400° F (+204.4° C)).

Hydraulic fluid MIL-H-83282A (for service between -50° F (-45.6° C) and +400° F (+204.4° C) is currently being introduced into military aircraft. The fluid has a synthetic hydrocarbon base and is fire-resistant.

OBJECTIVE

The objective of this project is to further examine compounded PNF vulcanizates as candidates for 0-rings for service between -50° F (-45.6° C) and +350° F (+176.6° C) in hydraulic fluid MIL-H-83282A.

INVESTIGATION

MATERIALS

A STATE OF

The six poly(fluoroalkoxy) phosphazene compounds examined are based on the same elastomer gum (PNF) which has the following general formula:

Superscripts refer to similarly numbered entries in the Technical References at the end of the text.

$$\begin{bmatrix}
\operatorname{OCH}_{2}^{\operatorname{CF}_{3}} \\
P = N \\
\operatorname{OCH}_{2}^{\operatorname{CF}_{2}} \\
\operatorname{OCH}_{2}^{\operatorname{CF}_{2}} \\
\end{bmatrix}_{n}$$

Three of the compounds were purchased from Horizons, under Contract N61533-75-M-3055 and two from Firestone under Contract N61533-75-M-2950. The sixth compound, designated NE-P-18 was supplied by Nichols Engineering, Inc., Shelton, Connecticut. The formulation of this compound is proprietary to Nichols. These six compounds represent the most advanced compounding technology for PNF. The Viton reference control was compounded at DTNSRDC and was chosen for its known stability to hot hydrocarbon hydraulic fluids. Formulations for the compounds are included in table 1.

The hydraulic fluid used in the immersion conditioning meets specification MIL-H-83282A and was supplied by Royal Lubricants as batch F8801.

TABLE 1
COMPOUNDS FORMULATIONS

A August and a second	Supplier							
Ingredient	DTNSRDC		Fireston.	Hori	Nichols			
	Compound Identification							
	Viton 1296	R194887	R194888	2104-44	2104-45	2104-46	NE-P-18	
Viton E-60-C	100							
PNF	100	100	100	100	-	-	- 1	
Quso WR82	30	30	100	100	100	100	100	
Nulock 321L		50	30	25	10	25	*	
Stan Mag ELC		6	6	10	40	10		
Elastomag 170		_0	0	_	-6	-		
Elastomag 20			4. — VI	-	0			
Maglite D	7			5		5		
Stabilizer (8-HQ) ₂ Zn		2	2			-		
Chemlink 30		-	2	, -	, -	-	*	
Silane A-172				1.5	1.5	-	*	
Teflon 6			6	_		2	*	
Calcium Hydroxide	6		0	A 150 100	, T	-		
Lucidol 78	_				, -	- I	*	
Luperco 101XL			111111	, -	1.5	-		
Vulcup R		0.36	0.36	1.5	(1 To 1	1.2	*	
Press Cure min/° F	60/320	24/340	24/340	15/350	15 (070	15 /750		
Oven Cure hr/° F	24/450	2.17 740	24/ 540	0.5/350	15/230 0.5/350	15/350		
* Proprietary.	- 17 100			0.5/550	0.5/350	0.5/350		

METHODS

Tensile properties were determined according to ASTM D 3196-73T. Values were calculated from the average cross sections and the average loads of five specimens. A forced draft oven was used for conditioning in hot hydraulic fluid. Fifty ml* of fluid covered 5 specimens suspended on a thin stainless steel wire in a 32×200 mm test tube. Specimens in the fluid were agitated daily.

Compression set was determined according to ASTM D395-69 Method B. Specimens consisted of stacked disks obtained when the tensile ring specimens were cut. The constant deflection rack was immersed in the hydraulic fluid and conditioned either in a forced draft oven or low temperature cold box.

The torsional stiffness of compounds was measured according to ASTM D1053-73. Iso-octane was the liquid medium for all temperatures except room temperature where air was the gaseous medium.

RESULTS AND DISCUSSION

Figure 1 clearly shows that the six PNF compounds cannot withstand continuous exposure to hydraulic fluid at +350° F (+176.6° C). Tensile strength deteriorates rapidly with immersion time. By contrast, the Viton reference control shows almost no change through the 14-day immersion period.

Data plotted on figure 2 shows that the six PNF compounds exhibit stability when heated for 14 days in the fluid at +300° F (+148.9° C), but continued immersion through 28 days shows a considerable loss in tensile strength. The Viton control shows little change through the 28 days immersion as observed previously. Although aircraft seals rarely experience high temperature in excess of two hours, the effects are cumulative over the life of the seals. Therefore, 28-day continuous immersion test is regarded as realistic.

Figure 3 illustrates the effect of increasing the immersion temperature from +300° F (+148.9° C) to +350° F (+176.6° C) on the strain energies of the six PNF compounds and the Viton control. The PNF vulcanizates deteriorated while the Viton was stable. Strain energy measurements are useful indicators of potential performance of materials under cyclic loading.

Ultimate elongations are generally stable through the 28-day immersion period at both +300° F (+148.9° C) and +350° F (+176.6° C) as shown in tables 2 and 3 on tensile properties.

^{*}A list of abbreviations used appears on page i.

TABLE 2 TENSILE PROPERTIES AFTER CONDITIONING IN MIL-H-83282A AT +300° F

Tensile		Supplier						
Properties	Immersion	DTNSRDC	Fire	stone	I	Iorizons	***************************************	Nichols
(ASTM	Time, days		Compounds					
D3196-73т)		Viton 1296	PNF 194887	PNF 194888	PNF 2104-44	PNF 2104-45	PNF 2104-46	PNF NE-P-18
Tensile strength, psi	0 3 7 14 28	1900 1800 1480 1490 1740	1540 1240 1130	1660 1530 1390 1330	1550 1310 1040 1080	1850 1670 1360 1290	2010 1560 1 510 1520	1090 910 930 860
% retained	28	35	720	880 53	520 34	1050 57	810 40	320 29
Ultimate Elon- gation, %	0 3 7 14 28	140 150 160 160 180	120 120 120 140 150	110 120 130 130 120	120 130 140 150 120	90 90 90 90 80	120 120 140 150	120 140 160 160
% retained	28	128	125	109	100	89	150 125	80 67
Strain Energy, in-lbs/in ³	0 3 7 14 28	1610 960 1270 1320 1880	680 610 575 540	900 780 810 820 640	780 700 630 690 300	710 700 540 490 400	940 650 810 880	660 630 770 780
% retained	28	116	79	71	38	56	620 65	180
Hardness, Shore A, points (ASTM D2240-68)	0	77	50	60	63	62	58	27 70

TABLE 3
TENSILE PROPERTIES
AFTER CONDITIONING IN MIL-H-83282A AT +350° F

Tensile		Supplier							
Properties	Immersion Time, days	DTNSRDC	Fire	stone		orizons		Nichols	
(ASTM			Compounds						
D3196-73T)		Viton 1296	PNF 194887	PNF 194888	PNF 2104-44	PNF 2104-45	PNF 2104-46	PNF NE-P-18	
Tensile strength, psi	0 3 7 14	1900 1910 1810 1800	1540 1310 1130 540	1660 1590 1280 790	1550 1070 650 310	1850 1420 1300 860	2010 1530 1070 560	1090 930 600 190	
% retained	14	95	35	48	20	47	28	17	
Ultimate Elon- gation, %	0 3 7 14	140 160 160 160	120 140 130 100	110 140 120 100	120 130 120 100	90 90 80 80	120 140 1 50 1 50	120 160 130 70	
% retained	14	114	83	91	83	89	125	58	
Strain Energy, in-lbs/in ³	0 3 7 14	1610 1660 1640 1560	680 670 600 240	900 1000 7 60 490	780 540 310 150	710 510 430 290	940 770 660 400	660 770 490 100	
% retained	14	96	35	54	19	40	42		
Hardness, Shore A, points (ASTM D2240-68)	0	77	50	60	63	62	58	15 70	

English Light stable

The six PNF compounds examined showed a significant improvement of the compression set over those examined in previous work, see table 4. However, from the stress-strain data cited above, it is expected that compression set, too, would suffer with increased conditioning time at +350° F (+176.6° C) in the hydraulic fluid.

TABLE 4 COMPRESSION SET (ASTM D 395-69 METHOD B)

Compound Identification	% Set After 7 Days Conditioning in MIL-H-83282A at -50° F at +350° F				
	at -50° F	at +350° F			
DTNSRDC Viton 1296	26	52			
Firestone R 194887 R 194888	9 1 9	65 69			
Horizons 2104-44 2104-45 2104-46	5 6 3	63 69 3 6			
Nichols NE-P-18	19	7 9			

Torsional stiffness data in figure 4 (items (a) and (b) show the superior low temperature flexibility of the PNF vulcanizates contrasted to the Viton compound.

Young's Modulus at room temperature was calculated from the torsional stiffness data and is shown in table 5. Viton 1296 has the highest modulus which is reflected in the Shore A hardness values shown in tables 2 and 3. The PNF compounds would exhibit higher moduli if they were compounded to a higher Shore A value. Generally, a Shore A value of 80 is considered about optimum for an 0-ring in this application. The PNF materials were between 50 and 70 in Shore A hardness contrasted to a value of 77 for the Viton.

TABLE 5 - YOUNG'S MODULUS AT ROOM TEMPERATURE (ASTM D 1053-73)

Supplier	Compound	Young's Modulus psi
DTNSRDC	Viton 1296	7470
Firestone	194887 194888	480 568
Horizons	2104-44 2104-45 2104-46	989 396 342
Nichols	NE-P-18	945

CONCLUSION

Future work on the sole PNF polymer available is not warranted for aircraft seal applications operating under temperature extremes of -50° F (-45.6° C) to $+350^{\circ}$ F (+176.6° C).

RECOMMENDATION

Until improved phosphazene or other polymers are developed, it is recommended that future efforts for high performance aircraft seal applications be directed toward the improvement of fluorocarbon compounds for low-temperature performance.

TECHNICAL REFERENCE

1 - Lagally, P., and W. Klemens, Elastomers for Service as Seals for Engine Lubricants and Hydraulic Fluids, NSRDC Rept MAT-74-42 (Oct 1974)

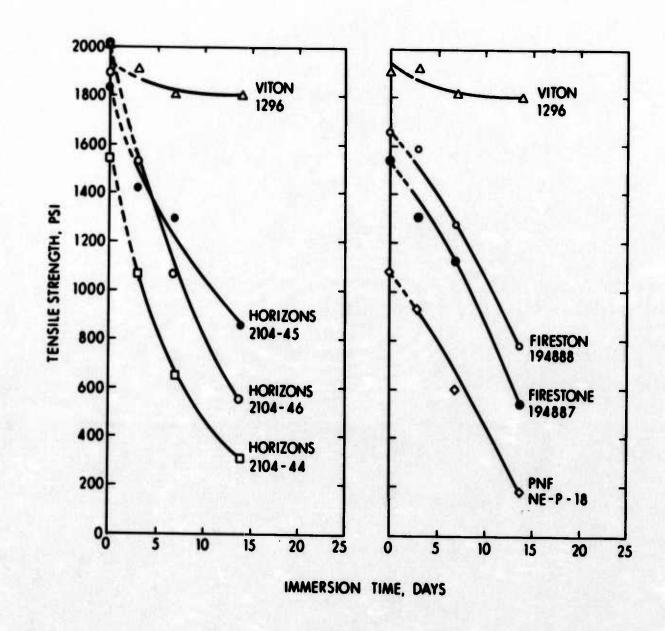


Figure 1 - Tensile Strength After Conditioning in MIL-H-83282A at +350° F

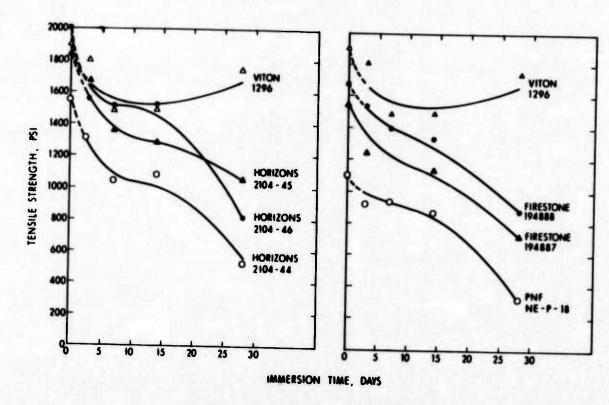


Figure 2 - Tensile Strength
After Conditioning in MIL-H-83282A at +300° F

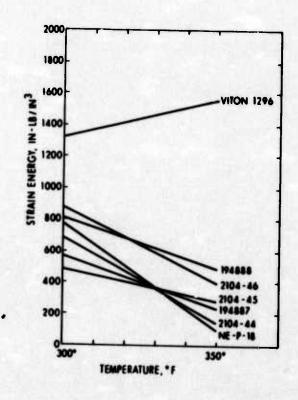
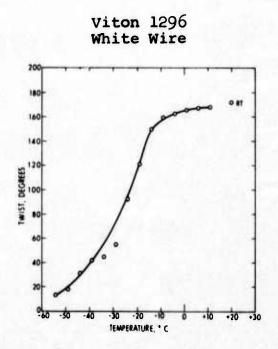
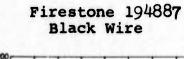
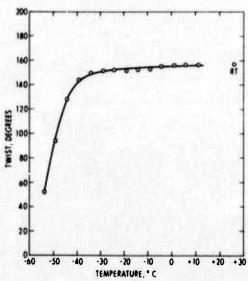


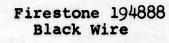
Figure 3
Strain Energy
Versus Temperature
14-Day Immersion
in MIL-H-83282A

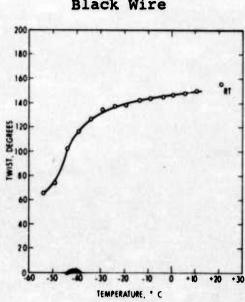












NE-P-18 Black Wire

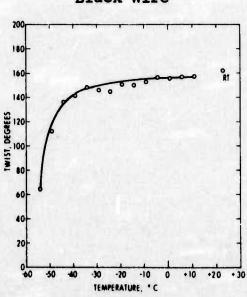


Figure 4
Torsional Stiffness (ASTM D 1053-73)

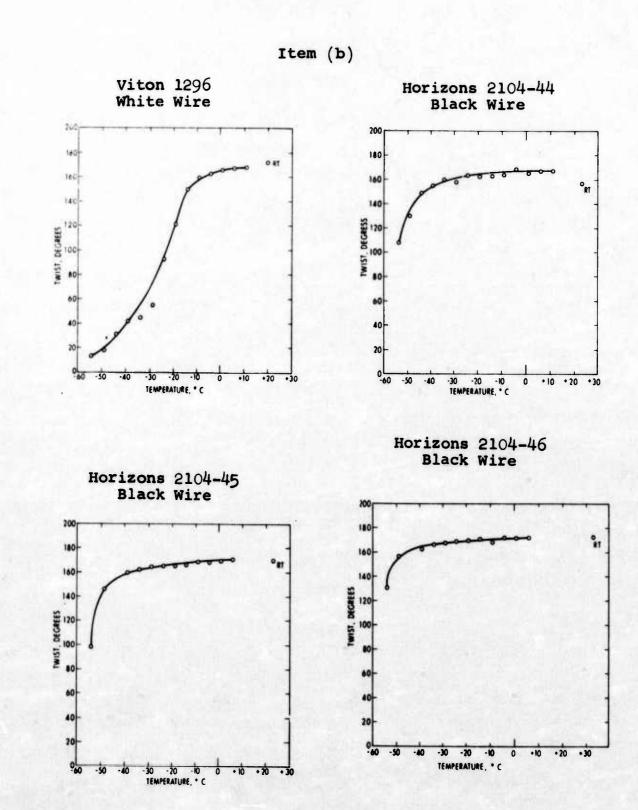


Figure 4 - Cont

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